



U.S. DEPARTMENT OF
ENERGY

Nuclear Energy

Modeling Used Fuel Storage Temperatures

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Thermal Model Development and Evaluation in Support of UFD Campaign

■ Why is it of concern to the campaign?

- Gap Analysis identified thermal profiles as a High Priority, NRC gap analysis in agreement
- Ranked #1 in Gap Prioritization because almost all degradation mechanisms are dependent on temperature

■ Realistic, not overly conservative, temperature profiles are needed

- Industry typically uses conservative models (limited conduction and convection, and simplifying assumptions) to assure that peak cladding temperature is within technical specifications

■ Over estimated temperatures will (to name a few):

- Over predict amount of hydride reorientation and radiation damage annealing
- Under predict the onset of potential deliquescence on the canister surface

Thermal Model Development and Evaluation in Support of UFD Campaign

- **Need accurate past, present, and future temperatures for clad and system components**
 - Especially critical for transportation, to know if we are at or below the ductile to brittle transition temperature during movement
 - Hottest fuel that could facilitate hydride reorientation will be the last to cool to the DBTT
 - Understanding temperature distribution throughout UF payload important to characterizing potential overall behavior characteristics

COBRA-SFS Development, Validation, and Application History

Code Development:

- **Early 1980's – DOE/OCRWM initiated a search for an analysis tool for accurate thermal prediction of spent fuel storage systems, to determine**
 - Peak fuel cladding temperature and assembly temperature distributions
 - Temperatures of system components related to safety (e.g., seals) to determine that they remained within design limits

- **Capability requirements were essentially “grand challenge” equivalent for CFD codes of the time, including**
 - Flow modeling within the fuel rod array
 - Steady-state natural convection cooling within the package and on the external boundary
 - Thermal radiation, which typically contributes over 20% of heat transfer within the package



COBRA-SFS Development, Validation, and Application History

- **COBRA-SFS and HYDRA-II selected from a survey of existing codes, as best available starting point for a multi-phase effort to**
 - Calibrate the codes for flow and heat transfer with inert gas (including thermal radiation) within rod arrays
 - Verify the implementation of the conservation equations (mass, energy, & momentum)
 - Validate against data from full-scale systems
- **Initial verification performed by comparison to single-assembly experiments, including**
 - Single PWR Spent Fuel Assembly tests at PNNL (PNL-5571, 1986)
 - Mitsubishi 15x15 PWR test assembly (Irino et al., 1986)
 - BNFL 16x16 PWR test assembly (Fry et al., 1983)
- **OCRWM Validation of COBRA-SFS at INL (cycle 3 of COBRA-SFS released)**



COBRA-SFS Development, Validation, and Application History

- **Validation consisted of performing “blind” pre-test predictions and post-test analysis of experiments at the Idaho National Laboratory’s Test Area North (TAN) facility**
- **Over 78 “blind” test analyses were performed, including**
 - Transnuclear TN24P (EPRI NP-5128 and PNL-5777 (Vol. I)), loaded with 24 spent fuel assemblies
 - Pacific Sierra Nuclear Associates’ Ventilated Concrete Cask (VCC) with Multi-Assembly Sealed Basket (MSB), loaded with 17 canisters containing consolidated spent fuel rods from 15x15 assemblies
 - Ridihalgh, Eggers, and Associates’ REA 2023 storage cask for BWR spent fuel

COBRA-SFS Development, Validation, and Application History

COBRA-SFS Validation:

■ Summary of COBRA-SFS V&V Analyses

- Single assembly (electrically heated) tests
 - EMAD Single Assembly (15x15) tests – Unterzuber, 1981
 - SAHTT (15x15 PWR assembly tests at PNNL) – PNL-5571, 1986
 - Mitsubishi 15x15 PWR test assembly – Irino et al., 1986
 - BNFL 16x16 PWR test assembly – Fry et al., 1983
- Multi-Assembly tests (with spent fuel)
 - CASTOR-V/21 (loaded with 21 PWR spent fuel assemblies from Surry) – EPRI NP-4887, 1980
 - REA 2023 cask (52 BWR spent fuel assemblies) – PNL-5777 (Vol. I), 1986
 - Transnuclear TN24P loaded with 24 spent fuel assemblies (from Turkey Point) – EPRI NP-5128, 1987 and EPRI NP-6191, 1987
 - Pacific Sierra Nuclear Associates Ventilated Concrete Cask (VCC) with Multi-assembly Sealed Basket (MSB), loaded with 17 canisters of consolidated rods from 15x15 assemblies – TR-100305 (EPRI), 1992.



COBRA-SFS Development, Validation, and Application History

Sample Results of COBRA-SFS V&V for Multi-Assembly Storage Cask (TN24P)

Image from EPRI NP-5128, 1987

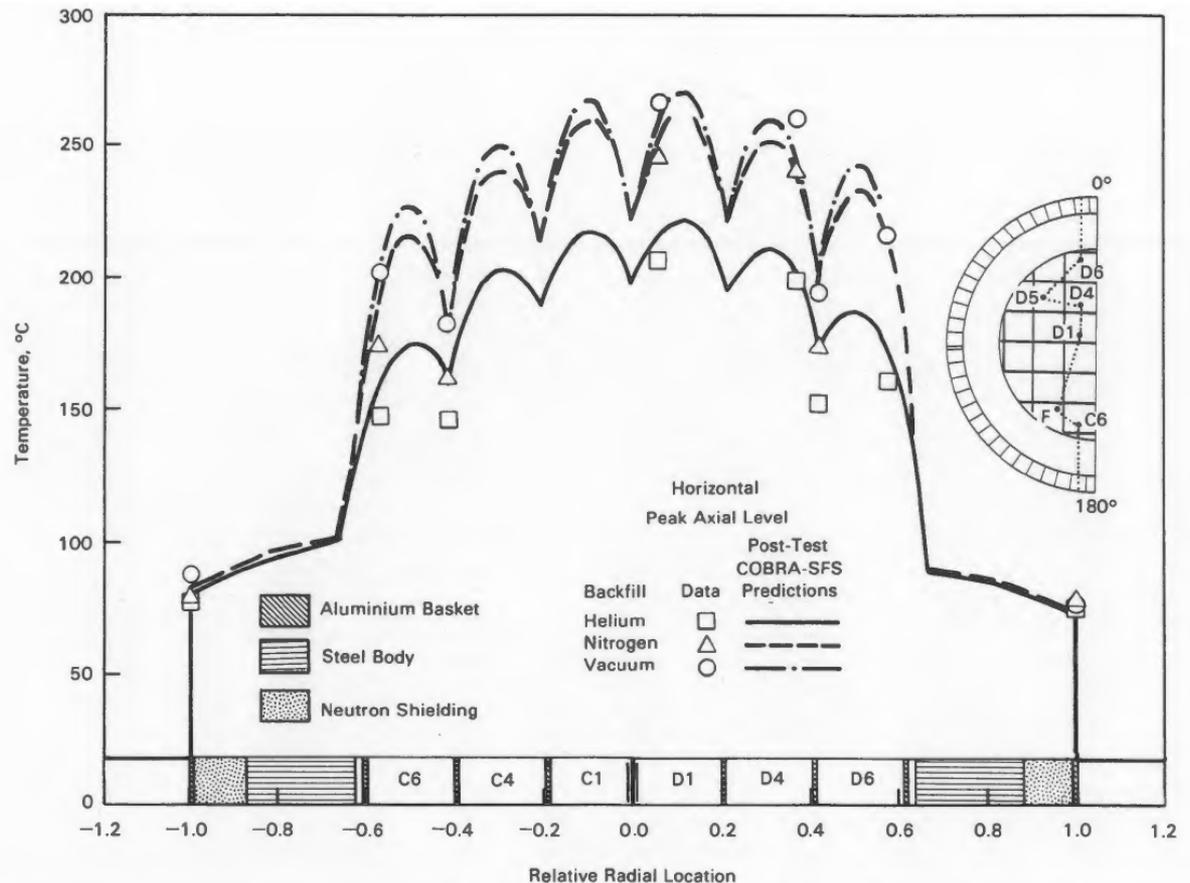


Figure 5-29. Post-Test Horizontal, Helium, Nitrogen, and Vacuum Radial Temperature Profile Predictions Compared to Test Data at Peak Temperature Axial Locations



COBRA-SFS Development, Validation, and Application History

Sample Results of COBRA-SFS V&V for Multi-Assembly Storage Cask (TN24P)

Image from EPRI NP-5128, 1987

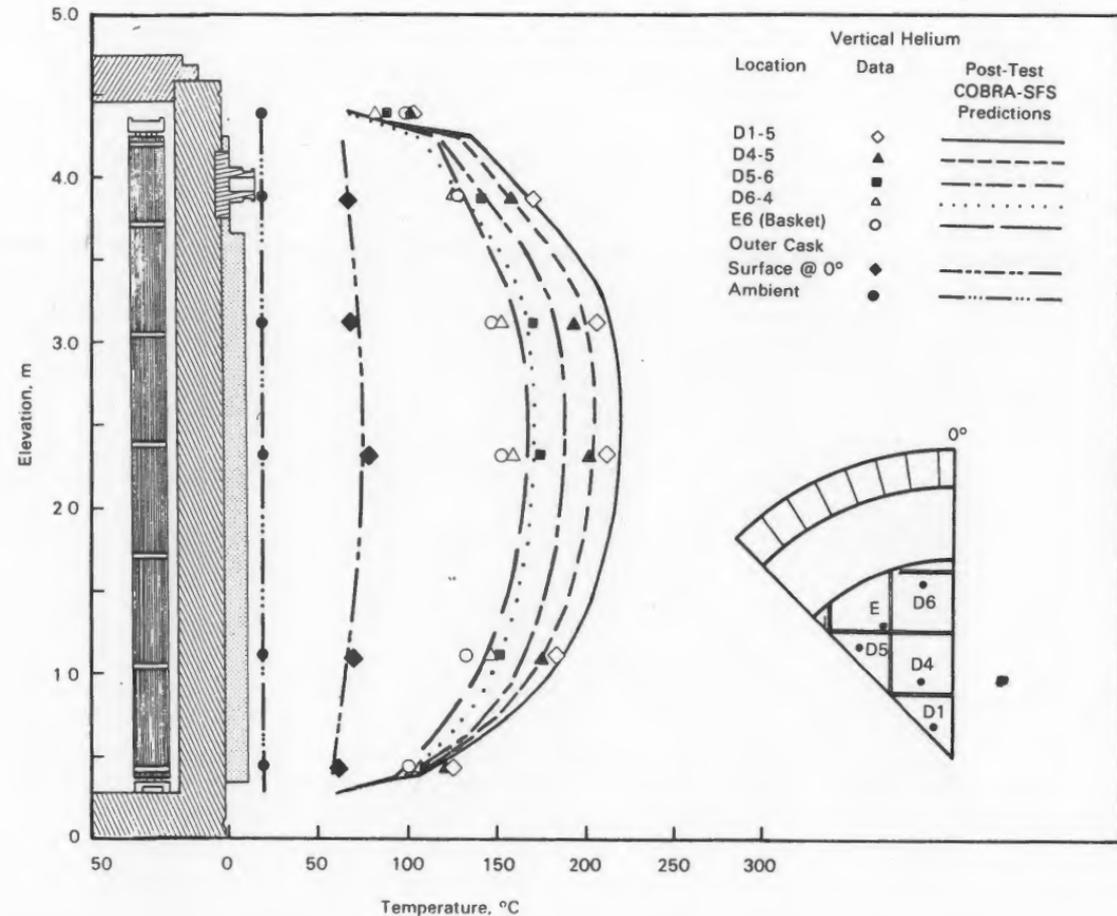


Figure 5-20. Post-Test Vertical, Helium Axial Temperature Profile Predictions Compared to Test Data

COBRA-SFS Development, Validation, and Application History

From Validation to Application:

■ DOE funded review by NRC of the COBRA-SFS code

- NRC subcontracted a team of national experts to review the code for use in predicting thermal performance of spent fuel storage/transportation systems

■ NRC establishes contract with PNNL to perform confirmatory analyses and review of applicant submittals (case work)

■ PNNL applies many other analytical codes, methodologies, correlation developments, however, all are verified via direct comparison back COBRA-SFS validation work

- Application of codes such as FLUENT, STAR-CD, STAR-CCM+, ANSYS, etc.
- Calibration of effective thermal conductivity (Keff) correlations for UF
- Correlations for enhanced Keff via pressurization of He in UF payload region

■ Additional codes beyond COBRA-SFS necessary as:

- Existing general purpose commercial codes are already in use by trained users
- COBRA-SFS requires seasoned operator and lacks pre- and post- GUI

COBRA-SFS Development, Validation, and Application History

Previous Applications:

- Duke power NUHOMS module relicensing support initiative
- EPRI funded dual purpose NAC cask performance evaluation
- Wire-wrap fuel feasibility evaluation for FFTF core
- Hanford Canister Storage Building
- Spent Fuel Pool analyses with postulated Zr fire
- Skull Valley Contention “H” rebuttal - model of field of Ventilated Vertical Concrete Storage Casks

COBRA-SFS Development, Validation, and Application History

Recent and Current Applications:

- **Numerous confirmatory analyses of Applicant's proposed Storage, Transfer, and Transport systems performed for NRC**
 - Normal and Hypothetical Accident Conditions
- **Extra regulatory fire evaluations**
 - Baltimore Tunnel Fire
 - Caldecott Tunnel Fire
 - MacArthur Maze Fire/Collapse
 - Newhall Pass Fire



Our Present UFD Campaign Goals and Objectives

- **Need to validate predictive tools for high burnup fuel and newer, higher capacity Dry Cask Storage Systems**
- **NRC asking Industry for inspections to support license renewal**
- **DOE teaming with EPRI (including supplying funding for future inspections)**
- **Pre-test and post-test thermal predictions performed on Calvert Cliffs Nuclear Power Station**

Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

Objectives:

- **Determine Storage System (Module, Canister, and Fuel Assembly) Component Temperatures**
- **Demonstrate “State of the Art” Evaluation Capability & Analytical Practices**
- **Perform Partial Verification (via comparison to measured canister temperature data to be gathered by Calvert Cliffs)**



Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

Calvert Cliffs Nuclear Power Station

Independent Spent Fuel Storage
Installation (ISFSI)



Ref. Google Maps



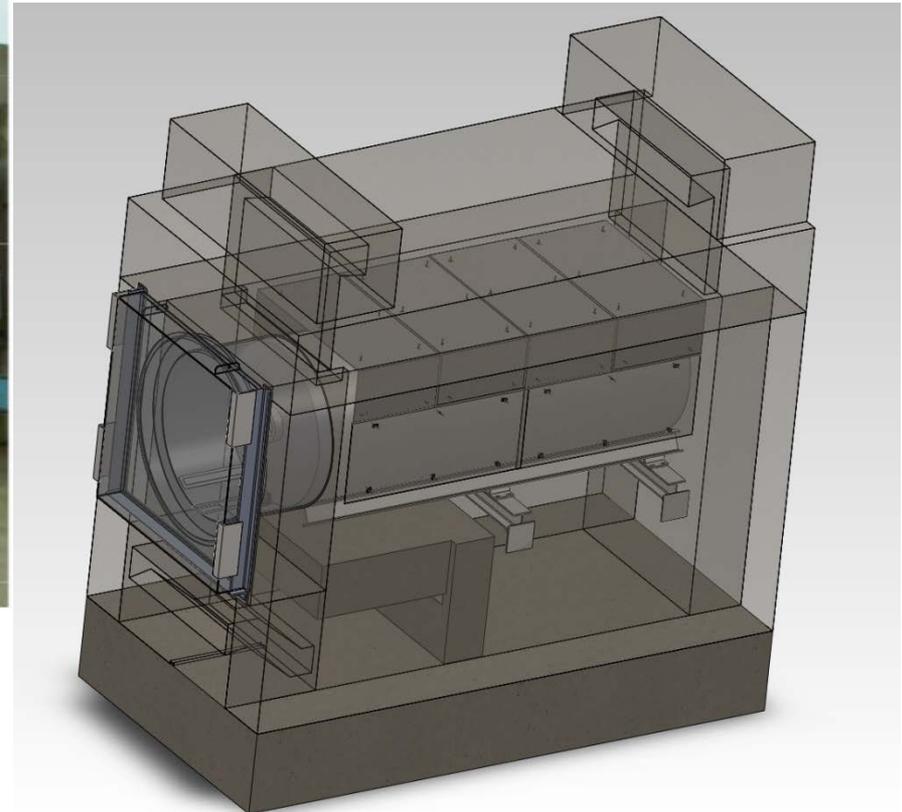
Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

Calvert Cliffs Site Specific NUHOMS Storage Module



Module front vent and doorway¹

SolidWorks® Model²



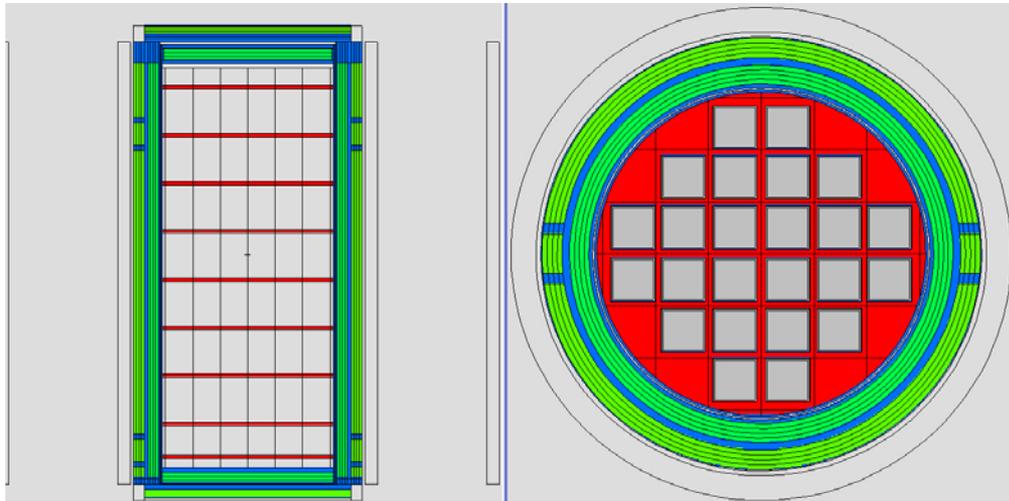
¹Ref. 'Jones 2010.ppt', Calvert Cliffs Dry Fuel Storage and Industry Lessons Learned

²SolidWorks® model provided by EPRI

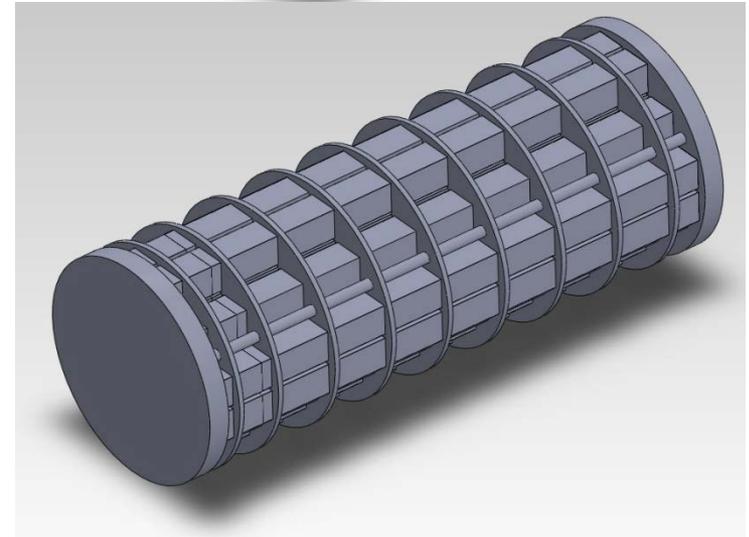
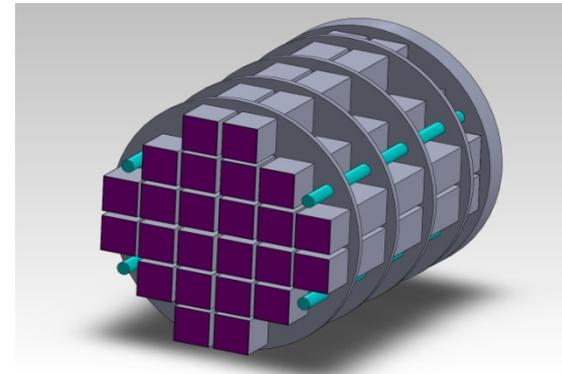


Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

DSC Details Extracted from MCNP Model and SolidWorks®



Ref. MCNP input model for DSC and transfer cask provided by John Massari, Calvert Cliffs

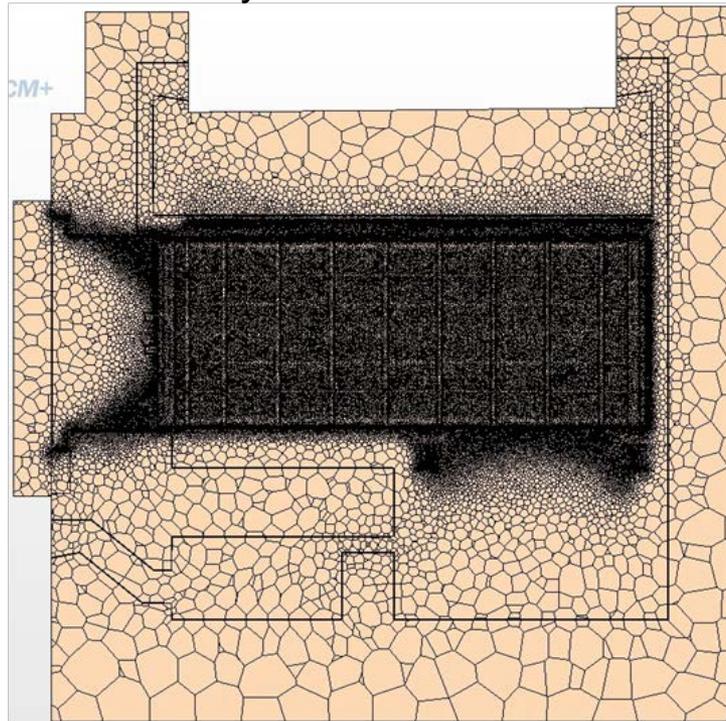




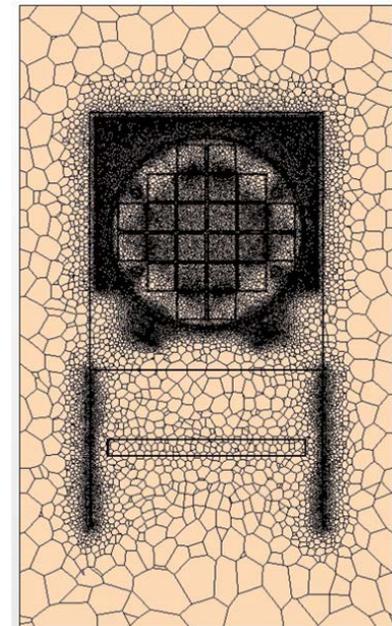
Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

■ Solid Model Primitives Transformed into STAR-CCM+[®] CFD Model and solved for HSM1 & HSM15 Temperature Distributions

- 43 separate regions connected by 117 interface boundaries
- SST (Menter) K-Omega Turbulence Model
- Flexible (all-y+) treatment for wall boundary conditions
- Default turbulent Prandtl #
- Default parameters in general
- 21,536,624 cells
- 127,598,563 faces
- 106,295,728 vertices

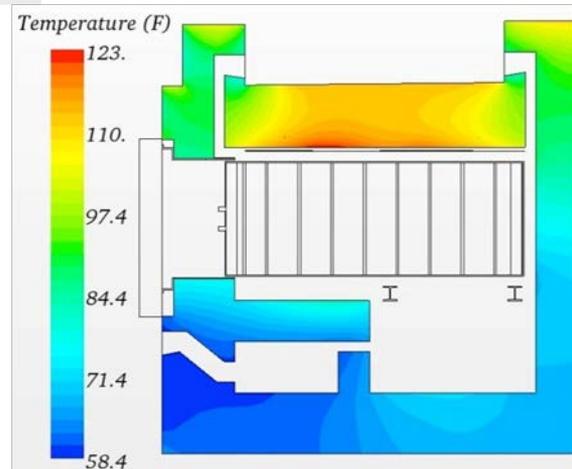
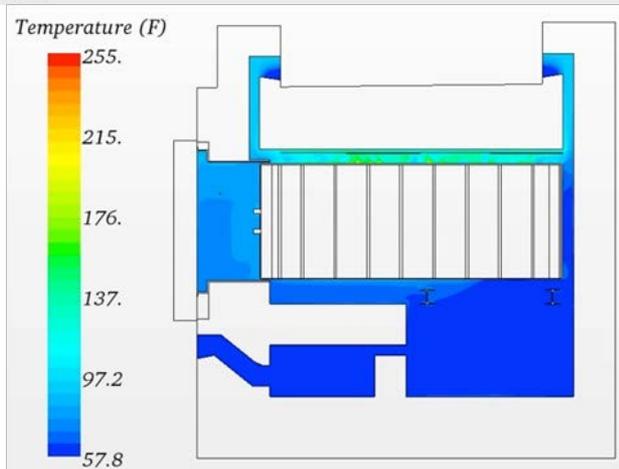
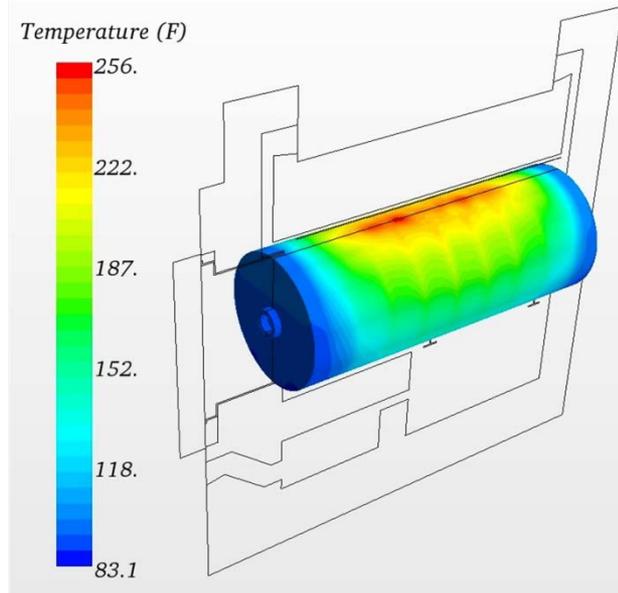
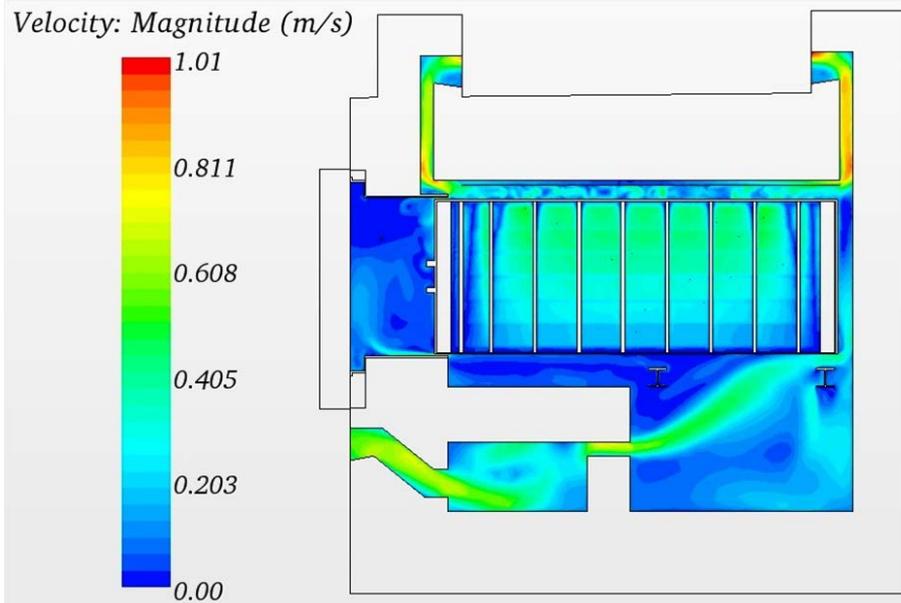


HSM15 Model Shown
(Lead Canister)





Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS



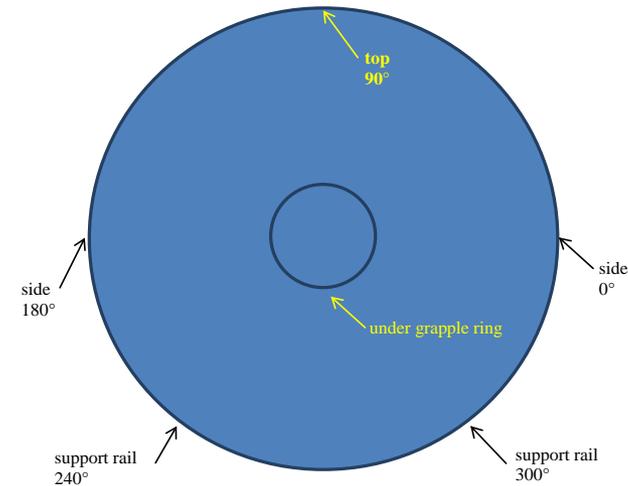
**Pre-test HSM15
Thermal Predictions
58°F (14°C) Ambient**



Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

■ How did pre-test predictions compare with collected data?

Temperature Location	Temperature (°F (°C))			
	TC measurement HSM-1	TC measurement HSM-15	CFD Model HSM-1	CFD Model HSM-15
Under Grapple Ring	112 (44)	124 (51)	100 (38)	110 (43)
Side (0°) – 0.0 in. (0.0 m)	108 (42)	n/a	100 (38)	110 (43)
Side (0°) – 20 in. (0.51 m)	109 (43)	n/a	116 (47)	133 (56)
Side (0°) – 40 in. (1.02 m)	108 (42)	n/a	136 (58)	164 (73)
Top (90°) – 0.0 in. (0.0 m)	115 (46)	n/a	103 (39)	114 (46)
Top (90°) – 20 in. (0.51 m)	117 (47)	n/a	142 (61)	180 (82)
Top (90°) – 40 in. (1.02 m)	119 (48)	n/a	178 (81)	242 (117)
Side (180°) – 0.0 in. (0.0 m)	104 (40)	n/a	100 (38)	110 (43)
Side (180°) – 20 in. (0.51 m)	105 (41)	n/a	115 (46)	135 (57)
Side (180°) – 40 in. (1.02 m)	108 (42)	n/a	134 (57)	167 (75)
Rail (240°) – 0.0 in. (0.0 m)	106 (41)	n/a	97 (36)	104 (40)
Rail (240°) – 20 in. (0.51 m)	107 (42)	n/a	101 (38)	112 (44)
Rail (240°) – 40 in. (1.02 m)	108 (42)	n/a	109 (43)	123 (51)
Rail (300°) – 0.0 in. (0.0 m)	105 (41)	n/a	97 (36)	104 (40)
Rail (300°) – 20 in. (0.51 m)	106 (41)	n/a	101 (38)	111 (44)
Rail (300°) – 40 in. (1.02 m)	106 (41)	n/a	109 (43)	122 (50)



■ Reasons for differences:

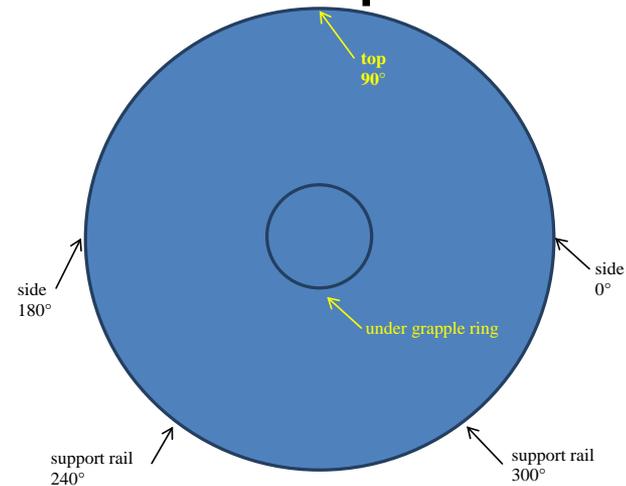
- Ambient 82°F (28°C) instead of seasonal average of 58°F (14°C)
- Canister end temperatures highly sensitive to fuel location and degree of contact
- Anomalous temperature data collected past 0.0 m insertion (measurement difficulties)
- Protective vent screens with smaller grids than modeled (larger pressure drop)



Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS

■ Taking these things into account, how do we compare?

Temperature Location	Temperature (°F (°C))			
	TC measurement HSM-1	TC measurement HSM-15	HSM-1 Model (post-test)	HSM-15 Model (post-test)
Under Grapple Ring	112 (44)	124 (51)	113 (45)	127 (53)
Side (0°) – 0.0 inches	108 (42)	n/a	113 (45)	127 (53)
Top (90°) – 0.0 inches	115 (46)	n/a	116 (47)	133 (56)
Side (180°) – 0.0 inches	104 (40)	n/a	113 (45)	128 (53)
Rail (240°) – 0.0 inches	106 (41)	n/a	107 (42)	118 (48)
Rail (300°) – 0.0 inches	105 (41)	n/a	107 (42)	118 (48)



■ Remaining reason for differences:

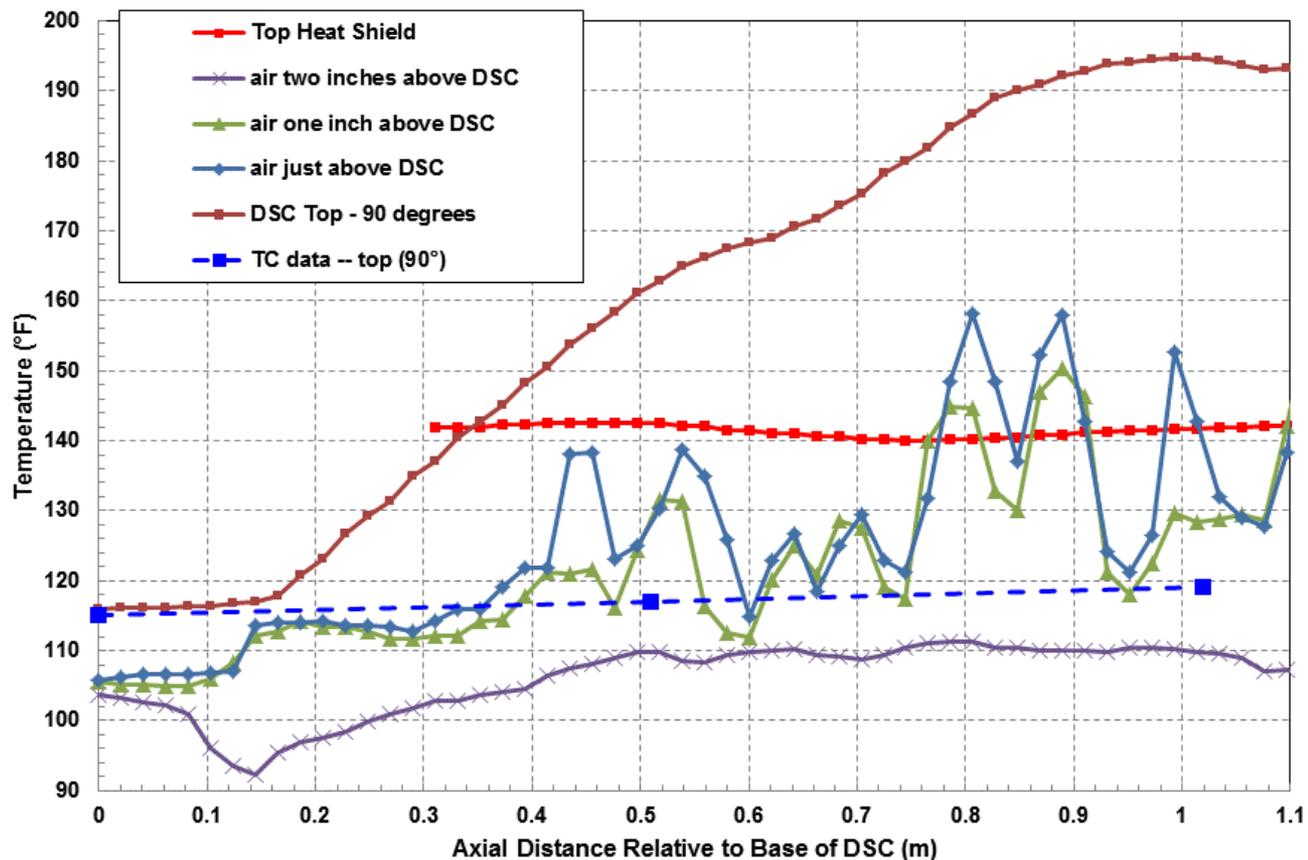
- Module door removed 40 minutes prior to taking outside measurements

■ Maximum component temperatures from CFD Models:

	Concrete temperature (°F (°C))	DSC temperature (°F (°C))	Fuel temperature (°F (°C))	Heat Shield temperature (°F (°C))
HSM-1 (Pre-test)	128 (53)	197 (92)	265 (129)	134 (57)
HSM-1 (Post-test)	133 (56)	208 (98)	279 (137)	143 (62)
HSM-15 (Pre-test)	145 (63)	278 (137)	402 (206)	166 (74)
HSM-15 (Post-test)	158 (70)	290 (143)	422 (217)	187 (86)



Thermal Predictions of HSM1 & HSM15 at Calvert Cliffs NPS



Axial Temperature Comparison for Top Heat Shield, Air Above DSC, and DSC Top Surface in HSM-1

Planned UFD Work

Nuclear Energy

- **Two EPRI inspections planned during FY13**
- **Sensitivity/Uncertainty analyses will be performed to identify important parameters to focus research efforts**
- **Extend CFD code validation**
- **Work with industry (demo) to validate codes during vacuum drying of HBU fuel under prototypic conditions**
- **Current codes can be extended from storage and transportation to disposal**
 - Hanford CSB as an example

Questions?

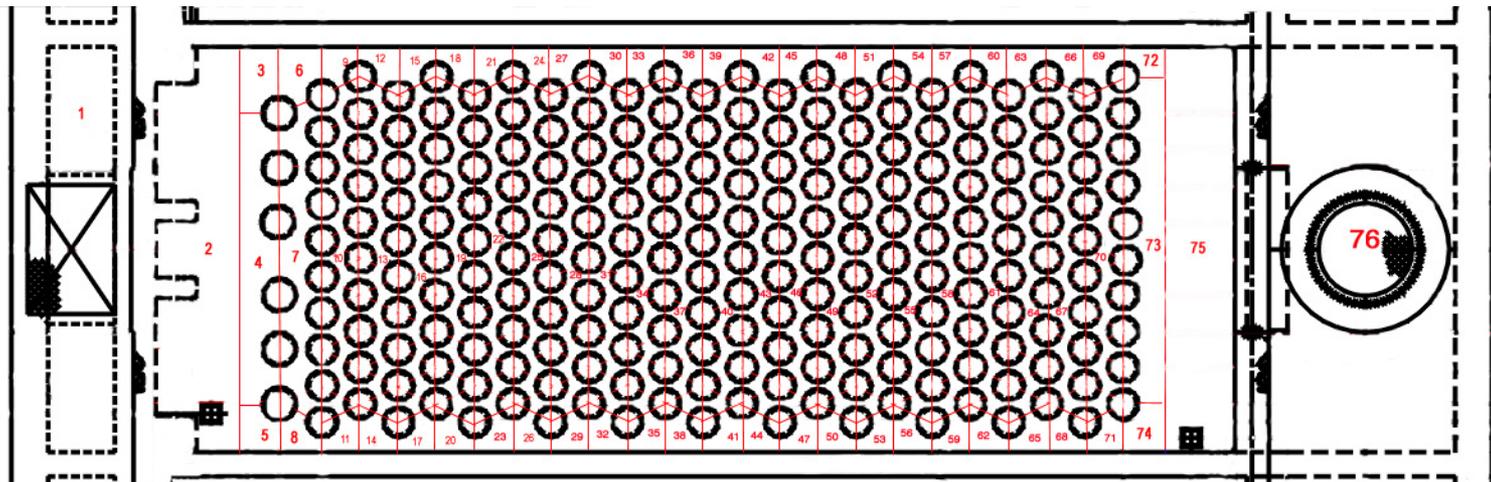


COBRA-SFS modeling of Canister Storage Building

- **Project W-464, IHLW Interim Storage Detailed Design (client: MacTec / CH2M Hill Hanford Group)**
- **Design-basis calculations for 150 kW heat load in Vault #2 of Canister Storage Building (CSB)**
- **Objective was to determine temperature distributions and magnitude and location of peak temperatures in**
 - IHLW glass,
 - stainless steel canisters,
 - steel storage tubes,
 - concrete walls of vault, and
 - circulating air within vault
- **Evaluated maximum heat load (150 kW) and low-heat load startup conditions**



Canister Storage Building Model



■ Vault #2 description:

- Triangular array of storage tubes, with up to 2 stacked canisters containing high-level waste glass per tube (up to 0.6 kW/canister)
- Cooled by natural circulation of air through underground concrete vault

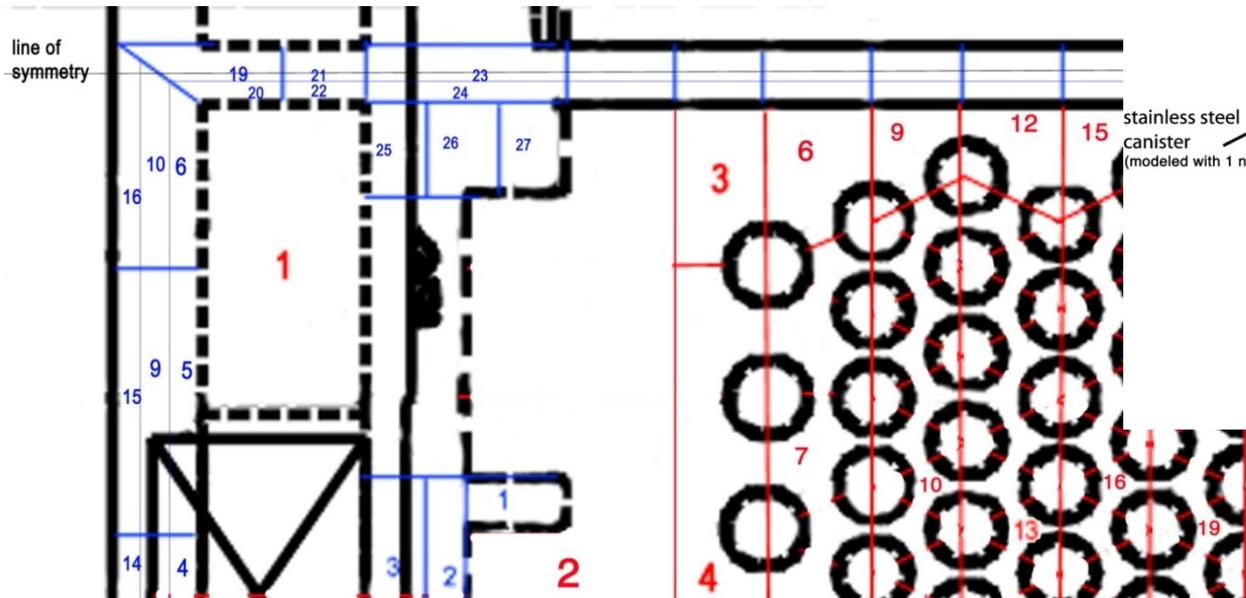
■ COBRA-SFS model:

- Detailed representation of canisters and flow paths through 'forest' of storage tubes
- Detailed representation of vault walls, storage tubes, canisters, and canister contents (glass)

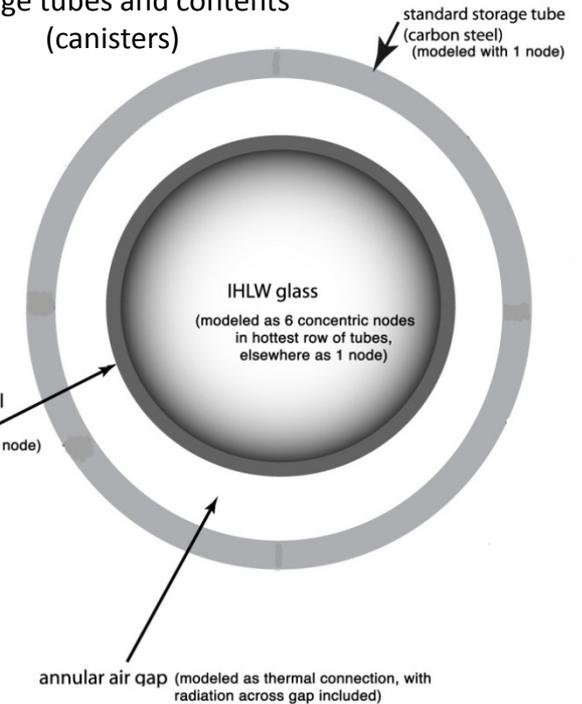


CSB Model Details

Note: conceptual diagrams; not to scale.



Example of noding detail for storage tubes and contents (canisters)



Example of noding detail for solid conduction nodes (blue) and flow paths (red)



COBRA-SFS V&V References

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