

**U.S. DEPARTMENT OF ENERGY  
OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT**

**PRESENTATION TO  
THE NUCLEAR WASTE TECHNICAL REVIEW BOARD**

**SUBJECT: CALICO HILLS RISK/BENEFIT  
ANALYSIS - SATURATED ZONE  
MODEL**

**PRESENTER: JACK ROBERTSON**

**PRESENTER'S TITLE  
AND ORGANIZATION: EXECUTIVE VICE PRESIDENT  
HYDROGEOLOGIC, INC.**

**PRESENTER'S  
TELEPHONE NUMBER: (703) 478-5186**

**DENVER, COLORADO  
MARCH 6-7, 1991**

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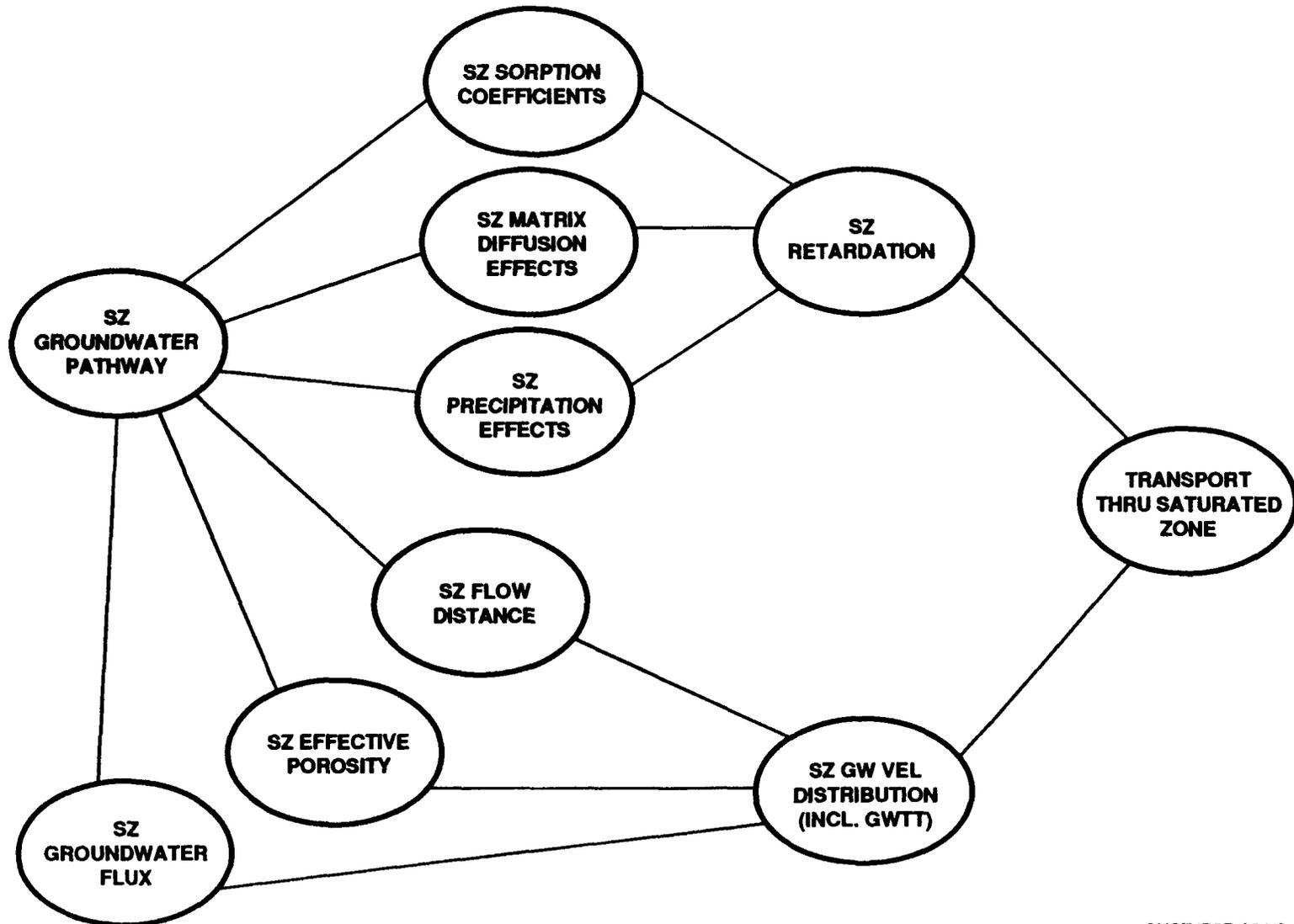
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# **SATURATED ZONE PERFORMANCE INTRODUCTION**

- **MULTIPLE BARRIER CONCEPT**
- **STATE OF KNOWLEDGE, SZ**
  - **FEW DATA**
  - **SCP CONSERVATIVE TRAVEL-TIME ESTIMATE**
- **CHRBA APPROACH TO SZ ASSESSMENT**
  - **REALISTIC BEST ESTIMATES**
  - **SORPTION/MATRIX DIFFUSION EFFECTIVE**
  - **RELEASE REDUCTION FACTOR, 10K YR**
  - **CUMULATIVE DISTRIBUTION PERCENTILES,  
99, 90, 50 AND 10**

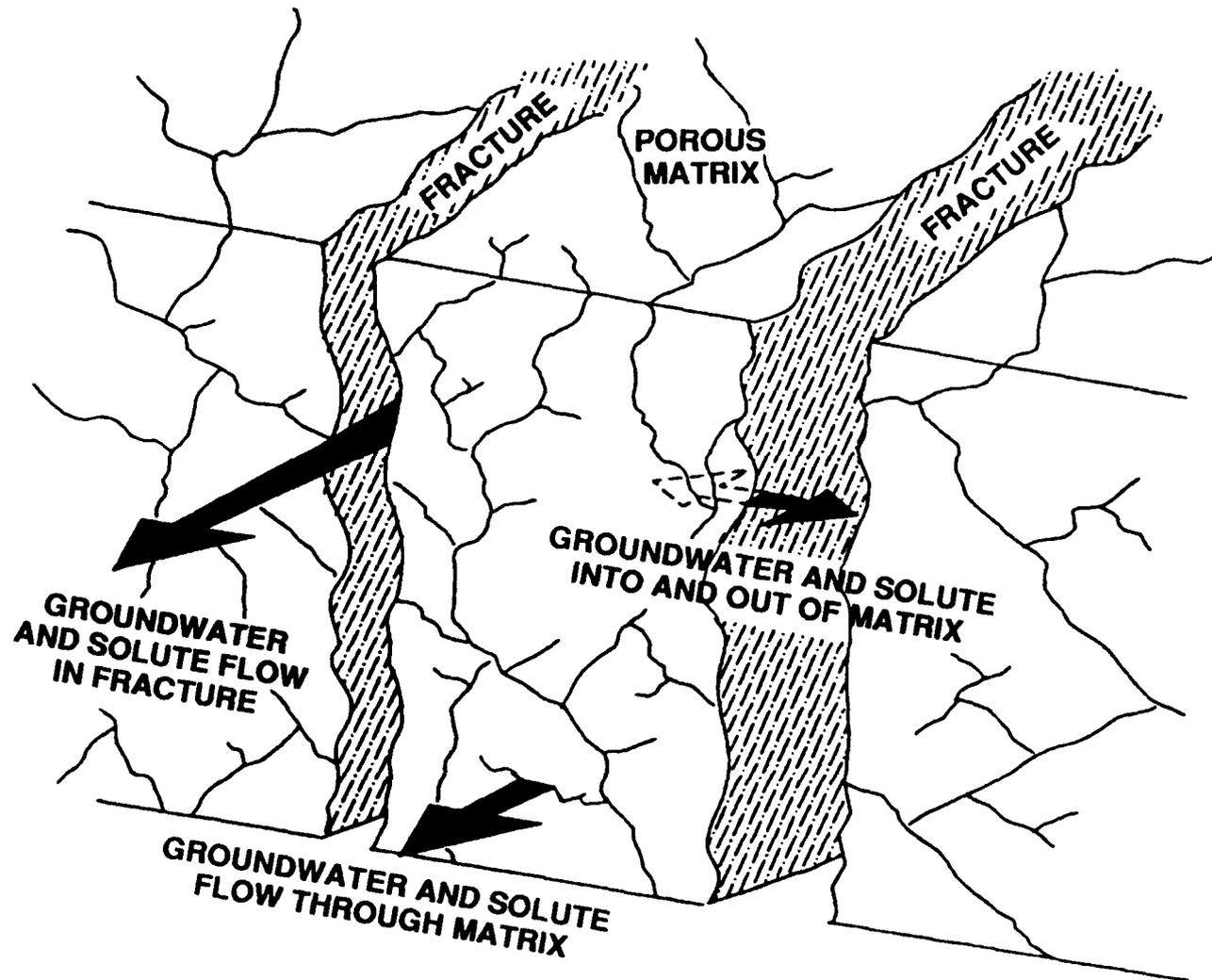
# SATURATED ZONE PERFORMANCE INFLUENCE DIAGRAM



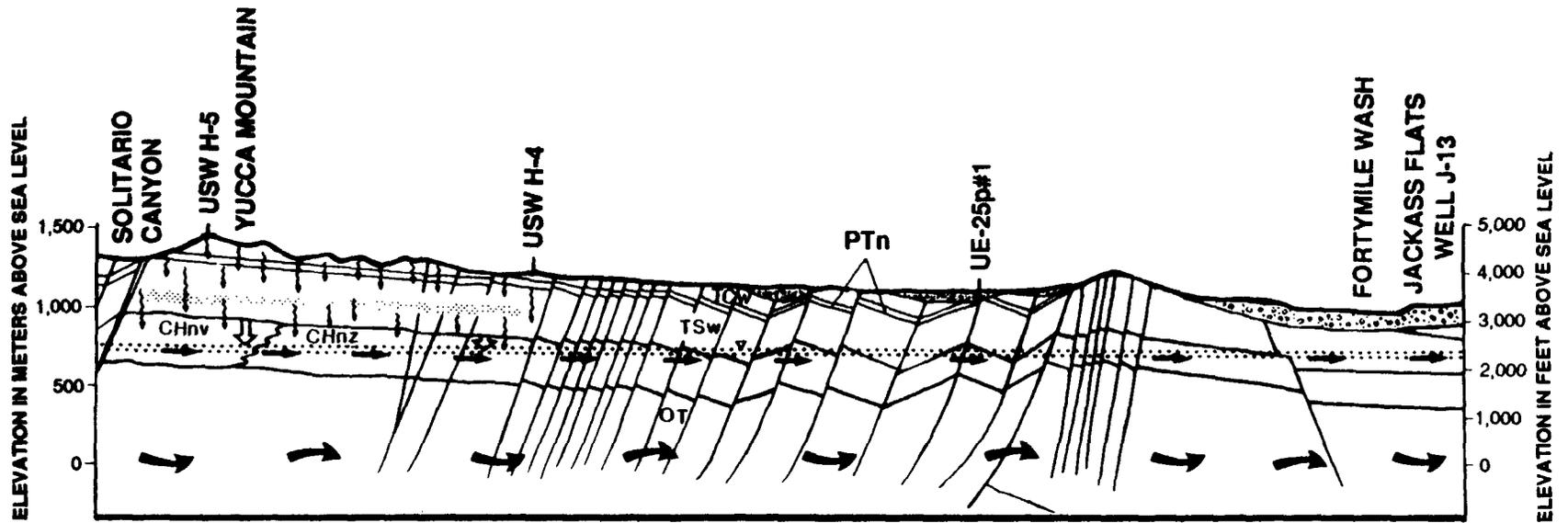
# **SATURATED ZONE CONSIDERATIONS BY CHRBA**

- **FLAT LATERAL GRADIENT**
- **UPWARD GRADIENT**
- **MOST OF PATHWAY IN CHnz**
- **FRACTURE PERMEABILITY AND FREQUENCY**
- **HYDRAULIC CONDUCTIVITY DECLINES WITH DEPTH**
- **HIGH BULK POROSITY**
- **HIGH ION EXCHANGE CAPACITY**
- **MUCH OF POROSITY PARTICIPATES IN FLOW AND TRANSPORT**
- **SMALL EFFECTS FROM CLIMATIC CHANGE**

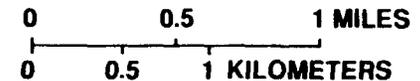
# GROUNDWATER AND SOLUTE FLOW AND DIFFUSION IN FRACTURED POROUS MEDIA



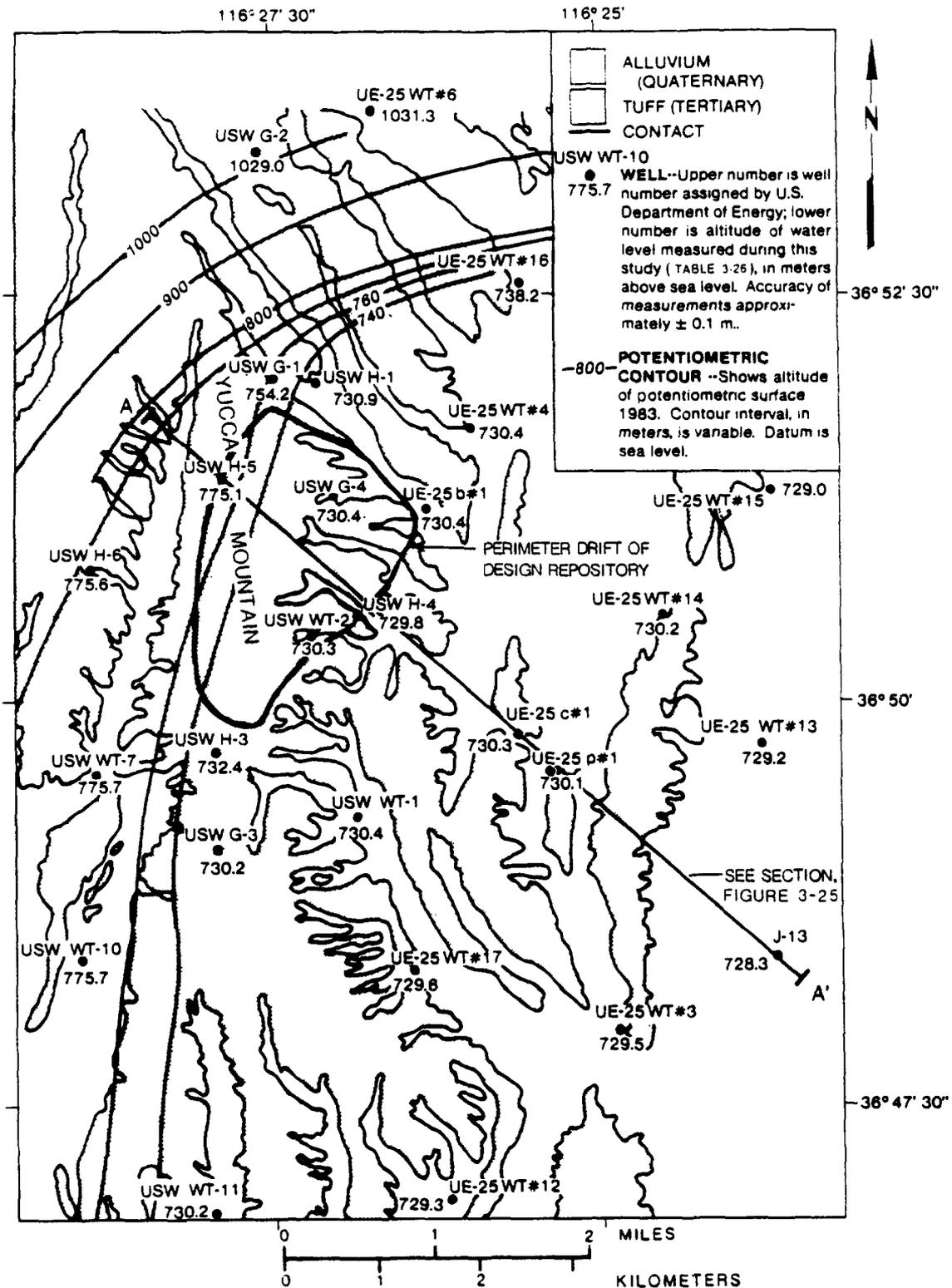
# CONCEPTUAL HYDROGEOLOGIC SECTION



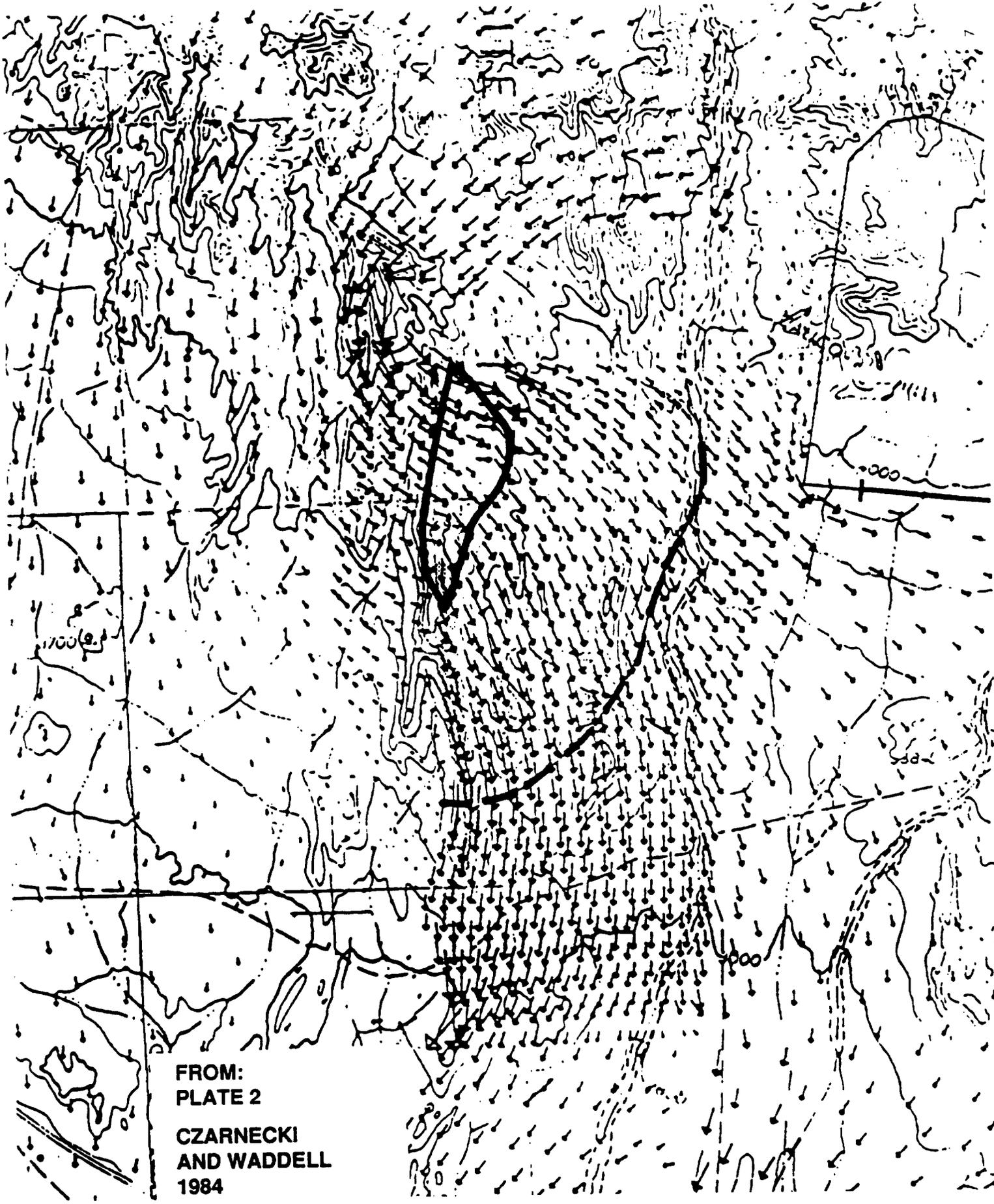
- |  |  |             |   |
|--|--|-------------|---|
|  | <b>ALLUVIUM &amp; TIMBER MOUNTAIN TUFF</b>   | <b>TCw</b>  | <b>TIVA CANYON WELDED UNIT</b>              |
|  | <b>DESIGN REPOSITORY<br/>(THICKNESS EXAGGERATED)</b>   | <b>PTn</b>  | <b>PAINTBRUSH NONWELDED UNIT</b>            |
|  | <b>WATER TABLE</b>   | <b>TSw</b>  | <b>TOPOPAH SPRING WELDED UNIT</b>           |
|  | <b>FLUX THROUGH THE UNSATURATED ZONE</b>   | <b>CHnv</b> | <b>CALICO HILLS NONWELDED VITRIC UNIT</b>   |
|  | <b>UNSATURATED-ZONE FLOW PATHS USED<br/>FOR TRAVEL TIME CALCULATIONS</b>                                 | <b>CHnz</b> | <b>CALICO HILLS NONWELDED ZEOLITIC UNIT</b> |
|  | <b>SATURATED-ZONE FLOW PATH FOR WATER THAT<br/>HAS PASSED THROUGH THE REPOSITORY LEVEL</b>               | <b>OT</b>   | <b>OLDER TUFF UNIT</b>                      |
|  | <b>DEEP SATURATED-ZONE FLOW PATHS FOR WATER<br/>THAT HAS NOT PASSED THROUGH THE<br/>REPOSITORY LEVEL</b> |             |   |



# PRELIMINARY COMPOSITE POTENTIOMETRIC-SURFACE MAP OF THE SATURATED ZONE



[From U.S. Department of Energy Site Characterization Plan, 1988, Figure 3-28 (modified from Robison, 1984; Robison, 1986).]



**FROM:  
PLATE 2  
CZARNECKI  
AND WADDELL  
1984**

# ESTIMATES OF RELEASE REDUCTION FACTOR REPRESENTING THE PERFORMANCE OF THE SATURATED ZONE PATHWAY (SIX CHRB PANELISTS)

<u>PROBABILITY LEVEL</u>	<u>GEOMETRIC AVERAGE REDUCTION FACTOR</u>	<u>ARITHMETIC AVERAGE REDUCTION FACTOR</u>
0.99	0.053	0.23
0.90	$1.0 \times 10^{-3}$	0.019
0.50	$4.6 \times 10^{-6}$	$1.7 \times 10^{-3}$
0.10	$1.5 \times 10^{-9}$	$1.7 \times 10^{-4}$

# POROSITY OF YUCCA MOUNTAIN TUFFS

<u>TUFF UNIT</u>	<u>BULK TOTAL POROSITY, %</u>	<u>SATURATED EFFECTIVE POROSITY, %</u>	<u>BASIS</u>	<u>REF.</u>
TOPOPAH SPRING	15 ± 5	8-12	CORE TESTS AND ESTIMATE	1
CALICO HILLS VITRIC	39 ± 8	20-30	CORE TESTS AND ESTIMATE	1
CALICO HILLS ZEOLITIC	30 ± 9	10-20	CORE TESTS AND ESTIMATE	1
		20	ESTIMATE	2
OTHERS	23 ± ?	5-15	CORE TESTS AND ESTIMATE	1

- REFERENCES: 1) SINNOCK et al., 1987  
 2) BARR AND MILLER, 1987

# BULK SATURATED HYDRAULIC CONDUCTIVITY/TRANSMISSIVITY, YUCCA MOUNTAIN TUFFS

<u>TUFF UNIT</u>	<u>MATRIX</u>	<u>BULK</u>	<u>BASIS</u>	<u>REF.</u>
TOPOPAH SPRING	3.5 x 10 <sup>-9</sup>	1 x 10 <sup>-3</sup>	CORE; WELL;	1
		5.7 x 10 <sup>-5</sup> -6.1 x 10 <sup>-3</sup>	WELL EST.	3
		8.1 x 10 <sup>-4</sup>	WELL	4
CALICO HILLS VITRIC	1.3 x 10 <sup>-6</sup>	2.4 x 10 <sup>-4</sup>	CORE; WELL	1
CALICO HILLS ZEOLITIC	4.2 x 10 <sup>-9</sup> 5 x 10 <sup>-9</sup> -3.5 x 10 <sup>-7</sup>	2.4 x 10 <sup>-4</sup>	CORE; WELL	1
		6 x 10 <sup>-4</sup>	CORE; WELL	4
		4.2 x 10 <sup>-3</sup> 1 x 10 <sup>-3</sup>	MODEL WELL	2 6
PROW PASS/ CRATER FLAT		2.3 x 10 <sup>-6</sup> -1.6 x 10 <sup>-3</sup>	WELL	4,6
OTHER	1.1 x 10 <sup>-7</sup>	4 x 10 <sup>-4</sup> -1 x 10 <sup>-3</sup>	CORE; WELL	1
		4.5 x 10 <sup>-6</sup> -4.2 x 10 <sup>-3</sup>	MODEL	2

# TRAVEL TIME ESTIMATES BY OTHERS

<b>CZARNECKI AND WADDELL (1984)</b>	<b>100 - 20,000 YRS <sup>1)</sup></b>
<b>SCP</b>	<b>170 YRS <sup>1) 2)</sup></b>

- 1) ASSUMES NO MATRIX DIFFUSION EFFECT**
- 2) ASSUMES FRACTURE FLOW ONLY  
(NO MATRIX FLOW)**

# ESTIMATED GROUND WATER AGES (C-14)

<u>APPARENT AGE</u>	<u>COMMENT</u>	<u>REFERENCE</u>
7,300 - 2,400 YR	AMARGOSA VALLEY	CLAASSEN, 1985
9,100 - 17,000 YR	YUCCA MOUNTAIN	CLAASSEN, 1985
2,280 - 17,000 YR	YUCCA MOUNTAIN	WADDELL et al., 1984
14,600 - 18,500 YR	YUCCA MOUNTAIN WELL USWH-6	BENSON AND McKINLEY, 1985

# TRAVEL TIME CALCULATION

GRADIENT (WELL H-4 TO WELL J-13) =  $2.7 \times 10^{-4}$   
(WELL USWWT-2 TO UE25WT#3) =  $1.6 \times 10^{-4}$

$K = 0.1$  TO  $1$  m/d

EFFECTIVE POROSITY =  $0.05$  TO  $0.3$  (ALLOWING FOR MATRIX DIFFUSION)

VELOCITY =  $5.4 \times 10^{-3}$  m/d  
TO  
 $5.3 \times 10^{-5}$  m/d

TRAVEL TIME FOR 5 km: 2,500 TO 260,000 YRS.

USING TYPICAL VALUES: (GRAD =  $2 \times 10^{-4}$ ,  $K = 0.2$ ,  
POROS =  $0.15$ )

$V = 2.7 \times 10^{-4}$  m/d  
TT = 50,000 YRS.

# SUMMARY ASSESSMENT OF SATURATED ZONE EXPECTED PERFORMANCE

- **LOW GRADIENT AND PERMEABILITY PLUS HIGH POROSITY CAUSE SLOW TRAVEL TIMES**
- **MATRIX DIFFUSION AND ION EXCHANGE CAUSE HIGH RETARDATION EFFECTS**
- **RELEASE REDUCTION FACTORS**
  - $10^{-3} - 10^{-2}$  @ 90%**
  - $10^{-6} - 10^{-3}$  @ 50%**
- **SZ VERY SIGNIFICANT POTENTIAL BARRIER**
- **RELATIVE IMPORTANCE OF CH<sub>n</sub> DIMINISHED BY SZ PERFORMANCE**

# REFERENCES

- 1) **SINNOCK, et. al., 1987**
- 2) **CZARNECKI, 1985**
- 3) **SCP, TABLE 3-8, 1988**
- 4) **SCP, TABLE 3-27, 1988**
- 5) **BARR AND MILLER, 1987**
- 6) **CRAIG AND ROBISON, 1984**